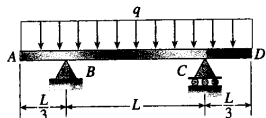


TAM 202, HW 13 SOLUTIONS, HW DUE ON 26th Nov, 2002, (prepared by Peeyush Bhargava)

4.5-9 Beam ABCD is simply supported at B and C and has overhangs at each end (see figure). The span length is L and each overhang has length L/3. A uniform load of intensity q acts along the entire length of the beam. Draw the shear-force and bending-moment diagrams for this beam.

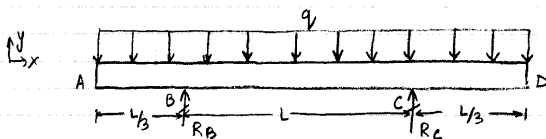


PROB. 4.5-9

Solution

Span length = distance between B and C = L.  
length of each overhang = L/3

FBD for beam ABCD.



By symmetry  $R_B = R_C = (5qL/6)$ .  
In gory detail:

$$\sum F_y = 0 = -q(L + \frac{L}{3} + \frac{L}{3}) + R_B + R_C$$

$$\text{or } R_B + R_C = \frac{5Lq}{3}$$

To find other equation to solve for reactions, do moment balance about B.

(Anticlockwise moments(+))

$$\sum M_B = 0$$

$$+ q(\frac{L}{3})(\frac{L}{6}) + R_C(L) - q(\frac{L}{3} + L)(\frac{L}{3} + L)\frac{1}{2} = 0$$

$$\text{or } R_C \cdot L = q \left( \frac{15}{18} L^2 \right)$$

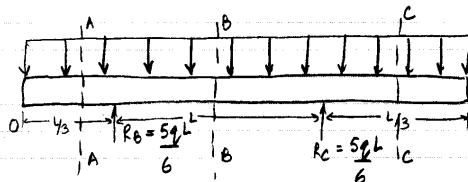
$$\text{or } R_C = \frac{5}{6} qL$$

As you could do by inspection

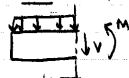
$$R_B = \frac{5Lq}{3} - \frac{5Lq}{6} = \frac{5Lq}{6}$$

Note: the moment due to a distributed load with constant magnitude is  $\frac{qx^2}{2}$  where q is the magnitude & x is the distance from the point about which moment is taken

To draw shear force diagram, start from either end and take cuts [i.e method of: FBD's]



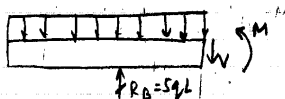
Cut A-A



$$\sum F_y = 0 \Rightarrow V = -qx \quad (\text{Linear function of } x \text{ with negative slope}) \quad \text{--- (1)}$$

$$M = -\frac{qx^2}{2} \quad (\text{quadratic function of } x \text{ with (-) slope}). \quad \text{--- (2)}$$

Cut B-B



$$\sum F_y = 0 \quad V = R_B - qx = \frac{5}{6} qL - qx = q \left( \frac{5L}{6} - x \right) \quad \text{--- (3)}$$

[ See that  $q = 0$  when  $x = \frac{5}{6}L$  the distance of this point from B =  $\frac{5}{6}L - \frac{L}{3} = \frac{L}{2}$  ]

$$\sum M = 0$$

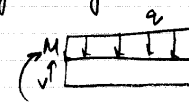
$$\Rightarrow M = \frac{5}{6} qL \left( x - \frac{L}{3} \right) - \frac{qx^2}{2}$$

$$M = -\frac{qx^2}{2} + \frac{5}{6} qLx - \frac{5}{18} qL^2 \quad \text{--- (4)}$$

M=0 will have 2 roots.

cut C-C can continue the same way by taking all the forces and moments

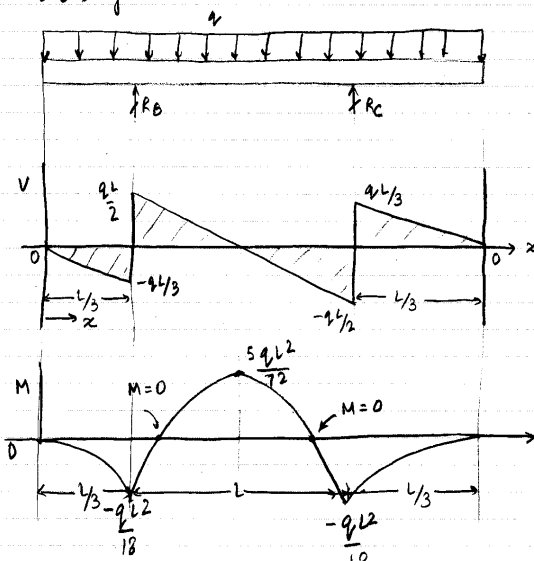
Or by starting over from the other side.



$$M = -\frac{qx^2}{2} \quad \text{--- (5)}$$

$$V = +qx \quad \text{--- (6)}$$

Using (1), (3), (6) Draw shear force diagram. Note: Diagram Not to Scale.



Use (2), (4), (5) to draw Bending moment diagram. Diagram NOT to scale.

Method 2:

Use the equations:  $\frac{dV}{dx} = -q$  & $\frac{dM}{dx} = V$ , integrate, find out  $V$  and $M$  in terms of  $x$  and  $V$  in terms of  $x$ .In this problem  $q = q_0$  (a constant).

$$\frac{dV}{dx} = -q \quad 0 \leq x \leq L/3$$

[ $x$  measured from  
left hand side].

Integrate,

$$V = V(0) - \int_0^x q dx = V(0) - qx$$

To calculate  $V(0)$ , use  $V=0$  at  $x=0$ , so  $V_0 = 0$ .

$$\text{so } V = -qx \quad 0 \leq x \leq L/3 \quad \text{--- (1)}$$

Similarly

$$\frac{dM}{dx} = V \Rightarrow M = \int_0^x V dx + M_0$$

$$\text{use } V = -qx \Rightarrow M = M(0) + \int_0^x (-qx) dx$$

$$\text{or } M = M(0) - \frac{qx^2}{2}$$

To calculate  $M(0)$  use  $M=0$  at  $x=0$ .

$$\Rightarrow M(0) = 0$$

$$\text{so } M = -\frac{qx^2}{2} \quad 0 \leq x \leq L/3 \quad \text{--- (2)}$$

See that the equation we got here is the same as when we took the cut A-A calculated  $V$  &  $M$ .

Now take  $\frac{L}{3} < x < \frac{4L}{3}$ . [have to take  $x$  in the region where there is no discontinuity in load or moment (no concentrated load or moment)]

So using the same equation  $\left[ \frac{dV}{dx} = -q, \frac{dM}{dx} = V \right]$ 

get

$$\left. \begin{aligned} \frac{dV}{dx} &= -q \\ \frac{dM}{dx} &= +V \end{aligned} \right\} \frac{L}{3} < x < \frac{4L}{3}$$

$$\text{Integrate for } V$$

$$V = V\left(\frac{L}{3}\right)^+ - \int_{L/3}^x q dx$$

$$\text{or } V = V\left(\frac{L}{3}\right)^+ - q\left(x - \frac{L}{3}\right)$$

$$\text{Now } V\left(\frac{L}{3}\right)^+ = -\frac{qL}{3} + \frac{5qL}{6}$$

$$V\left(\frac{L}{3}\right)^- \quad \uparrow \text{ jump in } V \text{ due to reactor at B (RB)}$$

$$V\left(\frac{L}{3}\right)^+ = \frac{qL}{2}$$

$$\text{so } V = V\left(\frac{L}{3}\right)^+ - qx + qL/3$$

$$V = \frac{qL}{2} + \frac{qL}{3} - qx$$

$$\text{or } V = \frac{5qL}{6} - qx \quad \text{--- (3)}$$

Integrate for  $M$ 

$$M = M\left(\frac{L}{3}\right)^+ + \int_{L/3}^x \left(\frac{5qL}{6} - qx\right) dx$$

$$\text{or } M = M\left(\frac{L}{3}\right)^+ + \frac{5qL}{6}\left(x - \frac{L}{3}\right) - \frac{q}{2}\left(x - \frac{L}{3}\right)^2$$

$$M\left(\frac{L}{3}\right)^+ = -\frac{qL^2}{18}$$

$$\text{so } M = -\frac{qL^2}{18} + \frac{5qL}{6}\left(x - \frac{L}{3}\right) - \frac{q}{2}\left(x - \frac{L}{3}\right)^2$$

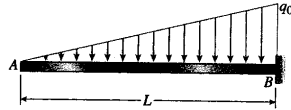
$$\text{or } M = -\frac{qx^2}{2} + \frac{5qLx}{6} - \frac{5}{18}qL^2$$

Similarly  $V$  &  $M$  can be determined for

$\frac{4L}{3} < x < \frac{5L}{3}$ , or can start over from the other side as done for method 1. Plot the bending moment & the shear force diagrams using equations found out. [of course, would be the same].

4-5-10

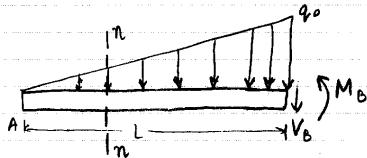
4.5-10 Draw the shear-force and bending-moment diagrams for a cantilever beam AB supporting a linearly varying load of maximum intensity  $q_0$  (see figure).



PROB. 4.5-10

Solution

FBD for the cantilever beam



$$\sum F_y = 0 \Rightarrow -V_B - (q_0 \cdot L) \frac{1}{2} = 0$$

$\frac{1}{2} (q_0 L) =$  Area of triangular region = magnitude of force.

$$\Rightarrow V_B = -\frac{q_0 L}{2} \quad \text{--- (1)}$$

$$\sum M_B = 0$$

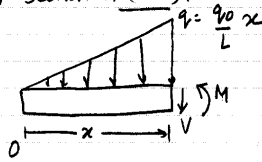
$$\Rightarrow M_B - \underbrace{\left(\frac{q_0 L}{2}\right)}_{\text{Magnitude of moment due to distributed load}} \left(\frac{L}{3}\right) = 0$$

$$\Rightarrow M_B = \frac{q_0 L^2}{6} \quad \text{--- (2)}$$

Now to draw shear force & bending moment diagram take a cut (n-n) & look at V & M.

Method 1

FBD for section A-(n-n).



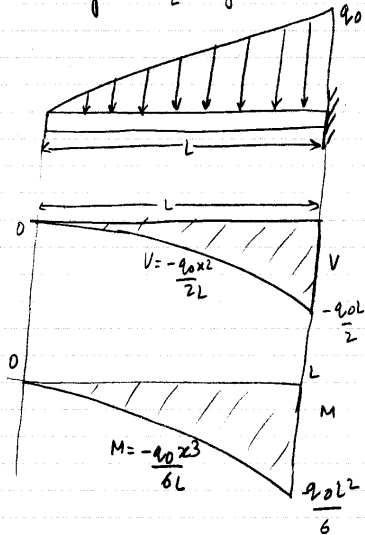
$$\sum F_y = 0 \Rightarrow V + \frac{1}{2} \left(\frac{q_0 x}{L}\right) (x) = 0$$

$$\text{or } V = -\frac{q_0 x^2}{2L} \quad \text{--- (3)}$$

$$\sum M = 0 \Rightarrow M + \frac{1}{2} \left(\frac{q_0 x}{L}\right) (x) \left(\frac{x}{3}\right) = 0$$

$$\Rightarrow M = -\frac{q_0 x^3}{6L} \quad \text{--- (4)}$$

Using (3) & (4), Draw shear force & bending moment diagram. [Diagrams not to scale]



Method 2.

Use  $\frac{dV}{dn} = -q$  &  $\frac{dM}{dn} = +V$ .

Here  $q$  is a function of  $x$ .

$$q = \frac{q_0 x}{L}$$

$$\frac{dV}{dn} = -\frac{q_0 x}{L}$$

$$V = V(0) - \int_0^x \frac{q_0 x}{L} dn$$

$$\text{or } V = V(0) - \frac{q_0 x^2}{2L}$$

$$V(0) = 0 \quad \because V = 0 \text{ at } x = 0.$$

$$\text{So } V = -\frac{q_0 x^2}{2L} \quad \text{--- (1)}$$

$$M = M(0) + \int_0^x V dx$$

$$\text{So } M = M(0) - \int_0^x \frac{q_0 x^2}{2L} dx$$

$$\text{or } M = -\frac{q_0 x^3}{6L} + M(0)$$

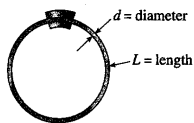
$$M(0) = 0 \quad \because M = 0 \text{ at } x = 0.$$

$$M = -\frac{q_0 x^3}{6L} \quad \text{--- (2)}$$

Use (1) & (2) to plot Bending moment & Shear force diagrams

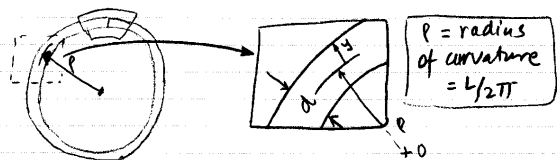
5-4-2

5.4-2 A copper wire having diameter  $d = 3 \text{ mm}$  is bent into a circle and held with the ends just touching (see figure). If the maximum permissible strain in the copper is  $\epsilon_{\max} = 0.004$ , what is the shortest length  $L$  of wire that can be used?



PROB. 5.4-2

Solution:  $d = 3 \text{ mm} = 3 \times 10^{-3} \text{ m}$   
 $\epsilon_{\max} = 0.004$



Now

$$\epsilon_{\max} = \frac{y}{R} = \frac{d/2}{L/2\pi} = \frac{\pi d}{L}$$

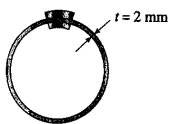
$$\Rightarrow L_{\min} = \frac{\pi d}{\epsilon_{\max}} = \frac{\pi (3 \times 10^{-3} \text{ m})}{0.004}$$

$$\text{or } L_{\min} = 2.36 \text{ m}$$

5-5-2

5.5-2 A thin strip of hard copper ( $E = 113 \text{ GPa}$ ) having length  $L = 2 \text{ m}$  and thickness  $t = 2 \text{ mm}$  is bent into a circle and held with the ends just touching (see figure).

(a) Calculate the maximum bending stress  $\sigma_{\max}$  in the strip. (b) Does the stress increase or decrease if the thickness of the strip is increased?



PROB. 5.5-2

Solution:

$$E = 113 \text{ GPa}$$

$$L = 2 \text{ m}$$

$$t = 2 \text{ mm} = 2 \times 10^{-3} \text{ m}$$

a) Calculate  $\sigma_{\max}$ .

$$\epsilon = \frac{y}{R} \Rightarrow \sigma = E\epsilon = \frac{E y}{R}$$

$$R = \text{radius of curvature} = \frac{L}{2\pi} \text{ and } y = t/2$$

$$\Rightarrow \sigma_{\max} = \frac{E(t/2)}{(L/2\pi)} = \frac{\pi E t}{L}$$

$$\text{or } \sigma_{\max} = \frac{\pi (113 \times 10^9 \text{ Pa}) (2 \times 10^{-3} \text{ m})}{2 \text{ m}}$$

$$\text{or } \sigma_{\max} = 355 \text{ MPa}$$

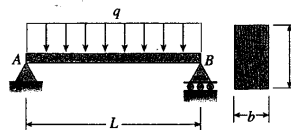
b)  $\sigma_{\max} \propto t$ .

If  $t$  increases,  $\sigma_{\max}$  increases.

5-5-4

5.5-4 A simply supported wood beam  $AB$  with span length  $L = 3.75 \text{ m}$  carries a uniform load of intensity  $q = 6.4 \text{ kN/m}$  (see figure).

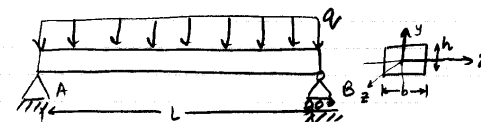
Calculate the maximum bending stress  $\sigma_{\max}$  due to the load  $q$  if the beam has a rectangular cross section with width  $b = 150 \text{ mm}$  and height  $h = 300 \text{ mm}$ .



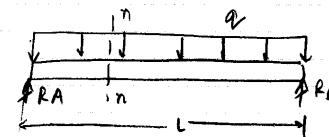
PROB. 5.5-4

Solution: The maximum bending stress occurs where the bending moment is maximum.

$$\text{So } \sigma_{\max} = \frac{M_{\max} y_{\max}}{I}$$



FBD for the beam.

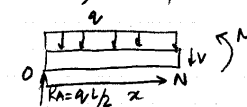


$$\sum F_y = 0 \quad R_A + R_B = qL$$

$$\sum M_B = 0 \Rightarrow -R_A L + \frac{qL^2}{2} = 0$$

$$\text{or } \begin{cases} R_A = \frac{qL}{2} \\ R_B = \frac{qL}{2} \end{cases}$$

take a cut, FBD for AN



$$\sum F_y = 0 \Rightarrow V = \frac{qL}{2} - qx$$

$$\sum M = 0 \Rightarrow M = \frac{qLx}{2} - \frac{qx^2}{2}$$

$M_{\max}$  occurs at  $\frac{dM}{dx} = 0$  or  $V = 0$

When  $V = 0$   $x = L/2$ .

$$M_{\max} = M(@ x = L/2) = \frac{qL^2}{8}$$

$$I = I_{xx} = \frac{1}{12} bh^3 \quad [\text{From Appendix D, pg 877}]$$

$$y_{\max} = h/2$$

$$\Rightarrow \sigma_{\max} = \frac{M_{\max} y_{\max}}{I_{xx}} = \frac{q \frac{L^2}{8} \cdot (h/2)}{\frac{1}{12} (bh^3)} = \frac{3qL^2}{4bh^2}$$

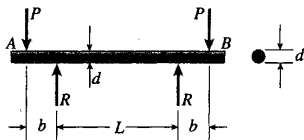
$$\text{or } \sigma_{\max} = \frac{3(6.4 \text{ kN/m})(3.75 \text{ m})^2}{4(150 \cdot 10^{-3} \text{ m})(300 \cdot 10^{-3} \text{ m})^2}$$

$$\text{or } \sigma_{\max} = 5 \text{ MPa}$$

5-5-6

5.5-6 A freight-car axle AB is loaded as shown in the figure, with the forces  $P$  representing the car loads (transmitted through the axle boxes) and the forces  $R$  representing the rail loads (transmitted through the wheels). The diameter of the axle is  $d = 80$  mm, the wheel gauge is  $L = 1.45$  m, and the distance between the forces  $P$  and  $R$  is  $b = 200$  mm.

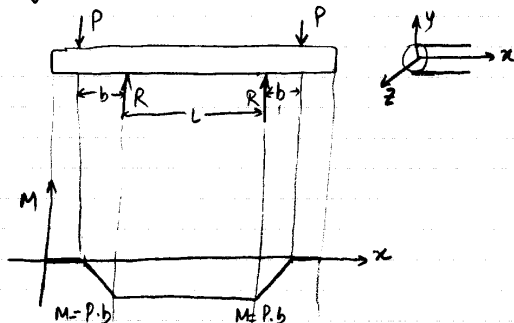
Calculate the maximum bending stress  $\sigma_{\max}$  in the axle if  $P = 46.5$  kN.



PROB. 5.5-6

Solution:  $R = P = 46.5 \text{ kN}$

The Bending moment diagram looks like this: -



$$M_{\max} = P \cdot b$$

$$y_{\max} = d/2$$

$$I = I_{xx} = \frac{\pi d^4}{64} \quad [\text{From Appendix D, 9 pg 879}]$$

$$\text{SO } \sigma_{\max} = \frac{M_{\max} y_{\max}}{I_{xx}} = \frac{P \cdot b \cdot d/2}{(\pi d^4/64)} = \frac{32 P b}{\pi d^3}$$

$$\text{or } \sigma_{\max} = \frac{32(46.5 \text{ kN})(200 \cdot 10^{-3} \text{ m})}{\pi(80 \cdot 10^{-3} \text{ m})^3} = 185.0 \text{ MPa}$$